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Soldering Alloys

S OLDERING ALLOYS include a wide range of alloying elements and properties. The common characteristics of these alloys is that they are used almost entirely for joining purposes, and that they have a liquidus (lowest temperature at which they are completely liquid) of less than 800 F, Table 1.

Solder Alloys

Tin-Lead: This is the largest single group and the most widely used of the soldering alloys. Most metals can be joined with these alloys. Joint clearances of 0.003 to 0.005 in. are recommended. Tin-lead solders are compatible for use with all types of base metal cleaners, fluxes, and heating methods.

Increasing the tin content of these solders produces better wetting and flow characteristics. Thus, when less tin is used, greater care should be exercised in surface preparation of the metals to be joined.

The highest melting-temperature solder in this group is that classified as 5A. This high-lead alloy is particularly suitable for use where operating temperature of the assembly may reach 300 F.

The most widely used solders—often referred to as generál-purpose solders—of the tin-lead system are the classifications 35A through 50A. They provide optimum wetting and flow properties, good strength at low temperatures, and require less preparation time.

The 60A solder, almost the eutectic, is particularly adaptable to delicate work or when soldering temperature may be critical. The solder with the highest tin content, 70A, is used for soldering zinc.

Tin-Lead-Antimony: These ternary alloys are generally used, with few exceptions, in the same applications as the tin-lead solders. They are not recommended for use on aluminum, zinc, or galvanized steel, however. The addition of antimony—up to a maximum of 6 per cent of the tin content—does not seriously affect the wettability or flow characteristics, but it does increase the mechanical properties. Joint-clearance recommendations are the same as for the tin-lead alloy system.

These solders have almost the same properties as equivalent tin-lead solders with about 5 per cent more tin. The physical properties—tensile, creep, and hardness—are higher than the non-antimonial alloys.

Tin-Antimony: The 95 per cent tin-5 per cent antimony solder has the best electrical properties of any solder alloy. In addition, it has high strength at temperatures to 300 F, and excellent flow characteristics.

Tin-Silver: The tin-silver alloys exhibit the same characteristics as the tin-antimony solders and are used for delicate instrument work.

Tin-Zinc: This group of alloys is not

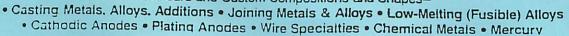
considered highly important for soldering applications. Widest usage is for soldering aluminum—primarily where lower soldering temperature than zincaluminum solders is required.

Lead-Silver: The physical properties of these solders—tensile, creep, and shear strengths—are good to 350 F. Fatigue properties are also better than the non-silver solder siloys. The silver-lead solders, however, have poor wetting characteristics and are subject to humid-atmosphere corrosion in storage. The addition of 1 per cent tin, replacing silver, increases wetting and flow, and re-

1			Table	1	ypical So	lders		
	ASTM Classification		Compo (per cent b)	Solidus	Temperature Liquidus	(F)
1	5A 10A		Tin 5	Lead 95 90		572 514	596 573	24
T	15A 20A			85 80		437 361	553 535	116 174
	25A 30A		15 20 25 30 35	75 70		351 351	511 491	150 130
	35A 40A			65		361 361	455	116 94
	45A 50A		45 50	55 50		361 361	441 421	80 60
	60A 70A		60 70	40. 30		361 361	374 378	13
ŀ	The second second	Tin	Antimony	Lead	14.31.16			
	20C 25C 30C	20 25 30	1.0 1.3 1.6	79.0		363 364	517 504	154 140 118
	35C 40C	35	1.8	68.4 . 63.2 58.0		364 365 365.	482 470 448	105
	-					300.	110	
	2.55	12nd 97.5	Silver- 2.5	Tin 1		579	- 579	. 0
	5.5S 1.5S	94.5 97.5	5.5 1.5	1.0		579 588	689 588	110
			Tin	Silver			•	
			96.5 95	3.5		430 430	430 473	43
			Tin	Zine				
			91 80	20		390	390 518	125
			70 60	40		390 390	592 645	202 255
	- '		30	70		390	708	318
			Cadmium 82.5	Zine 17.5		509	509	0
			40 10	90		509 509	635 751	126 241
	Tin	Indium	Blamuth	Load	Cadmium			
	8.3 12	19.1 21	44.7 48	22.6	9.6	117	117 136	0 0 7
	12.8 50	50	48	75.6	9.6	162 263	149 260	17
	48	52		1.	••	243	263	0

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duces susceptibility to corrosion. When tin is added to the lead-silver alloy, the silver content should be limited to 1.5 per cent, because, above this percentage, segregation occurs.

Cadmium-Zinc: The cadmium-zinc solders are useful in joining aluminum to itself or other metals. It is particularly useful in applications where service temperature is higher than allowed with the lower-meiting alloys.

Zinc-Aluminum: Designed decifically for soldering aluminum, zinc aluminum solders provide high joint straight with good corrosion resistance. A 5 per cent zinc, 5 per cent aluminum solder has been used without flux in electronics applications.

Indium Solders: Indium solders are used only in special applications, for instance, in cryogenic applications. The 50 per cent indium, 50 per cent tin alloy is particularly useful in glass-to-glass and glass-to-metal soldering.

Fusible Alloys: These bismuth-containing soiders are used where soldering must be performed at temperatures below 361 F. A representative group of these alloys is listed in Table 2. These solders are more sensitive to long-time loading above room temperatures (creep). The higher bismuth-content solders are not easily adaptable to high-speed soldering operations, nor do they easily wet the base metal.

Design Considerations

In designing for the use of the soldering alloys, little, if any, reliance should be placed on the strength of the solder. Instead, the joint should be designed to take advantage of the mechanical properties of the base metal by the use of such techniques as interlocking joints, edge reinforcing, or rivets.

No matter what type of mechanical

Table 2-Fusible Alloys

	11-		mattion	Temperature					
Alloy	Lend	Blamuth	Tin	Other	Solidus	Liquidus	Pasty Range		
Lipowitz Bending (Wood's	25.7	50	13.3	10 C4	158	158	0		
Metal)	25	50	12.5	12.5 Cd	158	165	7		
Eutectic	40	52		8 Cd	197	197	0		
Eutectic	32	32.5	15.5		203	203	0		
Rose's	28	50	22		204	229	25		
datrix dold and	28.5	48	14.5	9 Sb	217	140	223		
pattern	44.5	55.5			255	255	0		

method or device is used, there are basically only two types of joints—lap or butt—used in soldering. Lap joints are preferred because of the greater strength they impart to the assembly. Butt joints should be used only where sealing of the assembly is necessary.

Solder Forms and Shapes

Soldering alloys are commercially available in practically any desired shape, weight, or size. Typical examples of available forms are: Pig, slab, cake or ingot (rectangular or circular in shape), bar, paste, ribbon or tape (thicknesses of 1/16 to 3/16 in.), segment or drop (triangular bar or wire cut into pieces), pulverized or powdered, foil (thicknesses from 0.00125 in.), sheet (thicknesses from 0.010 to 0.100 in.), solid wire, flux core wire, and preforms.

Nonferrous Materials

Most of the nonferrous metals and alloys can be soldered. Table 3. Solderability depends on the alloy, the solders available, surface preparation, and soldering techniques. Some alloys require very special solders and/or fluxes

and carefully controlled production methods.

Aluminum and Aluminum Alloys: The soldering of aluminum differs from the soldering of brass, copper, steel, and most other common metals in several ways. The most important difference is that aluminum oxide forms a more tenacious and refractory oxide, making mandatory the use of corrosive fluxes designed for aluminum. A second difference is that the soldering of aluminum requires special techniques to produce flow into certain types of joints. Thirdly, the solder composition influences corrosion resistance of solder joints much more with aluminum than with copper. brass, or steel. With proper attention to details, however, a large variety of solder joints can be made in aluminum base materials.

The commonly soldered wrought-aluminum alloys are: 1060, 1100, 1145, 3003, 5005, 6061, 7072, and 8112 Table 4. Aluminum castings, by virtue of their composition, generally exhibit poor solderability.

The use of solders with high zinc or tin content is usually recommended. Table 5. The tin-lead solders are not recommended because the joint has poor

Table 3—Surface Preparation Requirements for Soldering Metals and Alloys

	Flux	Requireme	nts	
Metal or Alloy	Non- Currenty	Corresive	Special Flux and/or Solder	Re immended
Aluminum Aluminum-Bronze			X X	
Bervillum			x	
Beryllium Copper				.:
Brass		X		
Copper	X X			
Copper-Chromium	^	÷		
Copper-Nickei		X X X X		
Copper-Silicon		\$		
Gold	Y	^		
Incones	X X X			
Lead	x	x		
Magnesium			x	
fanganese-Bronze			^	
lones		x		x
Vickel		X		
Icnrome			x	
Platinum	X X			
liver	X	x		
tainiess Steel			x	
leer		x		
in	x	x		
In-Zinc	x	X X X		
Itanium				x
ne Die Geeren		x		
ne Die Castings			X	

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Table 4—Solderability of Aluminum Alloys

Alloy Group	Typical Alloy	Solderability	Recommended Flux			
1xxx (Commercial purity or higner)	1060 1100	Good	Chemical or reaction			
2xxx (Al-Cu)	2014	Fair*	Reaction			
JXXX (Al-Mn)	3003	Good	Chemical or reaction			
(AI-SI)	4043	Poor*	None			
SEEX! (Al-Mg) or (Al-Mg-Mn)	5005 5050, 5154 5456, 5083	Good Fair* Poor*	Chemical or reaction Reaction Reaction			
6xxx (Al-Mg-SI)	6061	Good*	Relation			
7xxxi (Al-Zn)	7072 7075	Good Poor	Reaction Reaction			
SEEX (Al-other)	8112	Good	Reaction			

[&]quot;Susceptible to intergranular penetration by solder. ISolderable only with abrasion or ultrasonic techniques and isolderability greatly affected by composition.

Table 5—Typical Solders for Aluminum

Composition (per cent)	Temper Solidus	ature (F) Liquidus	Density (1b per cu in.)	Wetting Ability on Aluminum	Flux Type Commonly Used	Relative Corresion Resistance
100 Zn	787	787	8.26	Good	Reaction	
95 Zn-5 Al	720 .	720	8.24	Good		Very Good
91 Sn-9 Zn	390	390	0.26	Fair	Reaction Chemical &	Very Good Fair
60 Sn-40 Zn	390	645	0.26	Good	reaction	
30 Sn-70 Zn	390	708	0.26	Good	Reaction Reaction	Good

Table 6—Solderability of Co	opper and Copper Alloys
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Metal	Solderability							
Coppers (Includes tough-pitch oxygen-free phosphorized, arsenical, silver-bearing leaded, tellurium, and selenium copper.)	Excellent. Need only rosin or other noncorrosive flux.							
Copper-tin alloys	Good. Easily soldered with activated rosin and intermediate fluxes.							
Copper-zinc alloys	Good. Easily soldered with activated rosin and intermediate fluxes.							
Copper-nickel alloys	Good. Easily soldered with intermediate and corrosive type fluxes.							
Copper chromium and beryllium-copper	Good. Require intermediate and corrosive type fluxes.							
Copper-silicon alloys	Fair. Silicon produces refractory oxides that require use of corrosive fluxes.							
Copper-aluminum alloys	Difficuit. May be soldered with help of very corrosive fluxes.							
digh-tensile manganese-bronze	Not recommended. Should be plated to insure consistent solderability.							

Table 7—Characteristics of Commonly Used Solders for Copper and Copper Alloys

Composition (per cent)	Temper Solidus	ature (F) Liquidus	Type and Uses
60 tin-40 lead	. 361	374	Quick-setting solder for fine electrical and tinsmith work.
50 tin-50 lead 95 tin-5 antimony	361 452	421 464	General purpose solder. Quick-setting solder whose creep strength at elevated temperatures is higher than that of the usual tin-lead solders. Especially useful for electrical joints and hotwater copper-tube lines that operate at temperatures up to 250 F.

resistance to corrosion and exhibits a loss of strength due to aging.

Copper and Copper Alloys: Copper is one of the easiest metals to solder. Nearly all solders and fluxes can be used in soldering copper—the choice depends primarily on intended application of the assembly. The relatively low temperatures required to solder copper permit joints to be made with a minimum of distortion, softening, and scaling of the work. Also, minimum damage occurs to electrical insulation and protected coatings. The solderability of copperbase alloys ranges from excellent to poor, Table 6.

There are no serious problems in soldering most of the copper-base metals. However, those alloys with beryllium, silicon, and aluminum require special fluxing. Also, copper-zinc alloys (brasses) should not be soldered with tin-antimony or tin-lead-antimony solders containing more than 1 per cent of antimony or 0.02 per cent of arsenic, Table 7. The excess antimony contributes to the brittleness of the joint and arsenic may

cause dewetting of the solder from the base metal.

Nickel and High-Nickel Alloys: Solder can be employed to join nickel and high-nickel alloys either to themselves or to any other solderable metals. Pure nickel and such alloys as Monei, K Monei, Permanickel, and Duranickel have good solderability. Alloys such as Inconel, Incoloy, Inconel X, and Nimonic 75 have fair solderability.

High-nickel alloys are usually specified because of their resistance to corrosive attack. When corrosion is a factor, the corrosion resistance of the solder alloy must also be considered. In some cases, the joint must be located so that the solder alloy will not be exposed to the corrosive environment. The higher tin content solders, such as 95 tin-5 antimony, usually are a better color match if appearance is important. However, the solder may oxidize in a different manner from the base metal and the joint may become noticeable after exposure.

On age-hardenable materials, the soldering should be done after aging. The temperature involved in soldering will not soften such metals as Duranickel, K Monel, and Inconel X, which have been fully age-hardened.

Any of the common types of solders may be used for joining the high-nickel alloys. It is usually desirable, however, to choose a relatively high-tin solder such as the 50 tin-40 lead or 50 tin-50 lead composition.

Zinc: Soldering of zinc is not difficult. Zinc - chlorice fluxes containing some hydrochloric acid are generally used along with a soldering iron with controlled heat. Zinc alloys, such as are used in die castings, normally contain aluminum and are difficult to solder. These must be treated as though they were an aluminum alloy, and aluminum soldering procedures should be followed.

Ferrous Materials

Iron and Steel—As with other metals, solderability of steel is influenced by its alloying constituents. The low-alloy or mild steels are most easily soldered. Medium—carbon steels (0.30-0.45 per cent C) solder less readily than low carbon (0.30 per cent C or less), and surface preparation is consequently more critical. High-carbon steels (over 0.45 per cent C) are seldom soldered.

Iron and steel corrode easily, and any rust or mill scale must be totally removed from the surface prior to soldering. A hot alkaline cleaner followed by an acid dip will generally produce good soldering surfaces. These metals are frequently precoated with lead, tin, or some other metal to provide good corrosion protection in addition * improved solderability.

Mildly corrosive fluxes are nec. ssary for soldering low-alloy steels. Special fluxes are available for the high-carbon steels and other materials such as stainless. Another important consideration is the necessity to provide absolutely clean surfaces prior to soldering.

Stainless: Commercially available leadtin solders can be used in joining stainless steels. Stainless steels are formulated to withstand corrosive attack and
are, therefore, difficult to flux chemically for soldering. Special highly corrosive stainless steel fluxes are used for
soldering these alloys. If the soldered
alloy is inaccessible and flux can't be
removed after assembly, pretinning of
parts may be necessary. Pretinning is
accomplished using a corrosive flux and,
after its removal, the parts may be assembled with a regular mild flux, thus
eliminating the corrosion problem.

Cast Iron: Cast iron contains graphite which cannot be wetted by molten solder. Special cleaning methods are often required for this material. Electrochemical cleaning, abrasion, and chemical cleaning are used to prepare cast iron for soldering. Care should be taken in heating the cast iron to avoid cracking. Ordinarily high-tin lead-tin solders are suitable for making the joint once the casting has been properly prepared.

Composition	Tie	Lord	Ant				Contract to the second	ren, I B X	Zinc, mex	Alumina	n, Arsoni max	Cadmien	Total of	metin	A LEANING
MARK	%	%	1 %	9		%	%	%	%	1 %	1 %	%	%		1
Sn96	Remainde	er 0.10, max			. 3.6 to		20	• •	0.005		0.05	0.005		(°F) 221 (430)	°G (°F) 221 (430
Sn70	69.5 to 71.5	Remaind	er 0.20 to 0.50	0.2			.0 80	ÒZ	0.005	0.005	0.03	0.001	0.08	183	193
Sn63	62.5 to 63.5	Remainde		0.2	5 0.0	15 0.0	0.0	02	0.005	0.005	0.03	0.001	0.08	183	(379)
Sn62	61.5 to 62.5	Remainde		0.2	1.75 to 2.25		18 0.1	02	0.005	0.005	0.03	0.001	0.08	179	179
- Sn60	59.5 to 61.5	Remainde	100000	0.25			0.0	12	0.005	0.005	0.03	0.001	0.08	183	(354)
Sn50	49.5 to 51.5	Remainde	The state of the s	0.25	0.01	5 0.0	B 0.0	12	0.005	0.005	0.025	0.001	0.08	183	(376) 216
Sn40	39.5 to 41.5	Remainder	-	0.25	0.01	5 C.08	0.0	2	0.005	0.005	0.02	0.001	0.08	183	238
Sn35	34.5 to 36.5	Remainder	A STATE OF THE STA	0.25	0.01	5 0.08	0.03	2	0.005	0.005	0.02	0.001	0.08	185	(460) 243
Sn30	29.5 to 31.5	Remainder		0.25	0.015	0.08	0.02		0.005	0.005	0.02	0.001	0.08	(365) 185	(469) 250
Sn20	19.5 to 21.5	Remainder	0.80 to 1.2	0.25	0.015	0.08	0.02		0.005	0.005	0.02	0.001	0.08	184	270
Sn10	9.0 to 11.0	*Remainder	0.20. max	0.03	1.7 to 2.4	0.08	•••	1	0.005	0.005	0.02	0.001	0.10	(363)	75181 25.
in5	4.5 to 5.5	Remainder	0.50, max	0.25	0.015	0.08	0.02	0	0.005	0.005	0.02	0.001	0.08	308	312
15	94.0. min	0.20, max	4.0 to 6.0	•••	0.015	80.0	0.08		0.03	0.03	0.05	0.03	0.03	235	240
Pb80 Re	mainder	78.5 to 80.5	0.20 to 0.50	0.25 -	0.015	0.08	0.02	0	.005	0.005	0.02	0.001	0.08	183	277
570 Re	mainder	68.5 to 70.5	0.20 to 0.50	0.25	0.015	0.08	0.02	0.	.005	0.005	0.02	0.001	80.0	351) 183	(531) 254
65 Rei	mainder	63.5 to 65.5	0.20 to 0.50	0.25	0.015	0.08	0.02	0.	005	0.005 .	0.02	0.001	0.08	361) 183	(489) 246
1.5	0.75 to - 1.25	Remainder	0.40, max	0.25	1.3 m 1.7	0.30	0.02	0.0	005	0.005	0.02	0.001	0.08 3	09	309
All the second s	0.25. max	Remainder	0.40, max	0.25	2.3 to 2.7	0.30	0.02	0.0	005	0.005	1.02	0.001	0.03	304	304
	0.25 max	Remainder	0.40, max	0.25	5.0 to 6.0	0.30	0.002	· 0.0	005	0.005	0.02	0.001		304	(579) 380

Yor information only.